

<b>Interview Summary</b>	<b>Application No.</b>	<b>Applicant(s)</b>
	09/685,718	ABRAMOV, YURI
	Examiner Thomas M. Dougherty	Art Unit 2834

All participants (applicant, applicant's representative, PTO personnel):

- (1) Thomas M. Dougherty. (3) \_\_\_\_\_.  
 (2) Ed Langer. (4) \_\_\_\_\_.

Date of Interview: 16 October 2002.

Type: a) Telephonic b) Video Conference  
 c) Personal [copy given to: 1) applicant 2) applicant's representative]

Exhibit shown or demonstration conducted: d) Yes e) No.  
 If Yes, brief description: proposed amendment.

Claim(s) discussed: 31.

Identification of prior art discussed: Yatsuda.

Agreement with respect to the claims f) was reached. g) was not reached. h) N/A.

Substance of Interview including description of the general nature of what was agreed to if an agreement was reached, or any other comments: \_\_\_\_\_.

(A fuller description, if necessary, and a copy of the amendments which the examiner agreed would render the claims allowable, if available, must be attached. Also, where no copy of the amendments that would render the claims allowable is available, a summary thereof must be attached.)

i) It is not necessary for applicant to provide a separate record of the substance of the interview(if box is checked).

Unless the paragraph above has been checked, THE FORMAL WRITTEN REPLY TO THE LAST OFFICE ACTION MUST INCLUDE THE SUBSTANCE OF THE INTERVIEW. (See MPEP Section 713.04). If a reply to the last Office action has already been filed, APPLICANT IS GIVEN ONE MONTH FROM THIS INTERVIEW DATE TO FILE A STATEMENT OF THE SUBSTANCE OF THE INTERVIEW. See Summary of Record of Interview requirements on reverse side or on attached sheet.

THOMAS M. DOUGHERTY  
 PRIMARY EXAMINER  
 GROUP 2100  
 2834

  
 Examiner's signature, if required

Examiner Note: You must sign this form unless it is an Attachment to a signed Office action.

Continuation of Substance of Interview including description of the general nature of what was agreed to if an agreement was reached, or any other comments,

It was agreed that the following proposed claim language overcomes the extant rejection: "A weighted SAW inter-digital transducer (IDT) having at least two internal electrode fingers shaped and arranged with a predetermined periodicity, each of said fingers having a shape defining a ratio between its width and its arrangement-periodicity, and also defining variable spacing between each of said fingers, such that said ratio varies substantially along each of said fingers, said variable ratio inducing SAW velocity dispersion along said fingers, thereby providing a weighting mechanism to control weighting coefficients for achieving desired frequency characteristics of the IDT.

Applicant's new independent claim (Sep.23, 2002)

34. A weighted SAW inter-digital transducer (IDT) having at least two **internal** electrode fingers shaped and arranged with a predetermined periodicity, each of said fingers <sup>having a shape</sup> defining a ratio between its width and its **arrangement-periodicity**, such that said ratio varies substantially along each of said fingers, said **variable** ratio inducing SAW velocity dispersion along said fingers, thereby providing a weighting mechanism to control weighting coefficients for achieving desired frequency characteristics of the IDT.

Table 1. Regarding the independent claim 4(rejected), 24(rejected), 34 (new).

Row No	Prior Arts (including Yatsuda's Disclosure)	Applicant's Disclosure
1	<p style="text-align: center;"><b><u>Tapered IDT</u></b></p> <p>The whole IDT and the fingers are similarly tapered to achieve a ratio <math>w(y)/p(y) = \text{Constant}</math>, thereby providing a substantial absence of <b>SAW velocity dispersion</b>, where <math>w(y)</math> is the finger's width along their length and <math>p(y)</math> is the periodicity arrangement of the fingers.</p>	<p style="text-align: center;"><b><u>IDT Weighted By Novel Mechanism</u></b></p> <p>A <b>variable</b> ratio, for example in Applicant's Fig. 3, results the finger shapes <b>substantially different</b> from the shape of the overall IDT. The fingers are trapezoidal, while the IDT is substantially rectangular.</p>
2	<p style="text-align: center;"><b><u>Tapering As A Weighting Mechanism</u></b></p> <p>Yatsuda illustrates periodicity of fingers grating in Fig. 2, where the overall IDT is tapered. The periodicity is changed from <math>P_H</math> to <math>P_L</math>, i.e. from high periodicity to low periodicity.</p> <p>A periodicity tapering causes that the voltages between fingers are distributed with different periodicity from top to bottom of the "fan-type" IDT.</p> <p>A tapered IDT provides weighting, because distribution of voltages between fingers varies in periodicity from top to bottom.</p>	<p style="text-align: center;"><b><u>Velocity Dispersion As A Weighting Mechanism</u></b></p> <p>The disclosed SAW IDT is weighted by the novel mechanism of SAW velocity dispersion.</p> <p>When SAW velocity is dispersed along <b>internal</b> fingers, we get the effect of different time-delay of SAW beams, propagating in different SAW tracks for each <math>y</math>.</p> <p>The time-delay distribution causes a phase weighting of the SAW tracks distributed along the fingers. The distributed phase weighting is utilized for weighting coefficients definition.</p>

<p><b>3</b></p> <p>The frequency characteristic of a "fan-type" IDT (Applicant's Fig. 2b) having tapered fingers is calculated by:</p> $A_{25}(\omega) = E(\omega) \sum_{n=1}^N p_n \int_{-L/2}^{+L/2} \exp(-j(\kappa_0)x_n(y)) dy \quad (3)$ <p>where</p> <p><math>p_n</math> is a polarity of the <math>n^{\text{th}}</math> finger: <math>p_n = (-1)</math>, if <math>n^{\text{th}}</math> finger is grounded, and <math>p_n = (+1)</math>, if <math>n^{\text{th}}</math> finger is hot;</p> <p><math>\kappa_0</math> is a SAW wave number, <math>\kappa_0 = \omega/V</math>, <math>V</math> is a <b>constant</b> SAW velocity for each <math>y</math>, because of the <b>constant</b> ratio <math>w(y)/p(y)</math>;</p> <p><math>x_n(y)</math> is the <b>X</b>-coordinate of <math>n^{\text{th}}</math> finger's center.</p> <p>The weighting is achieved by the varying of the fingers positions via <b>Y</b>-coordinate.</p> <p>The SAW velocity dispersion effect is <b>NOT</b> a degree of freedom for weighting for such an IDT.</p> <p>The same words are relevant to the equivalent prior art fan-type/tapered IDT, shown in Fig. 2 by Yatsuda.</p>	<p>The frequency characteristic of the IDT having trapezoidal fingers is:</p> $A_{30}(\omega) = E(\omega) \sum_{n=1}^N p_n I_n \exp(-j\kappa_0 x_n) \quad (4a)$ <p>where the weighting coefficients <math>I_n</math> vary with finger number <math>n</math>, <b>ONLY if the SAW velocity dispersion effect is present</b>.</p> <p>Now, the SAW wave number is dispersed along <b>Y</b>-coordinate: <math>\kappa_0 + \kappa(y)</math>, and the weighting coefficients <math>I_n</math> are calculated via the dispersion <math>\kappa(y)</math>.</p> <p>Control of the values <math>I_n</math> due to <b>varying</b> the fingers' shapes, which substantially different from the shape of the overall IDT, is the <b>novel degree of freedom</b>, and is the essence of the disclosure.</p> <p>An example calculation of frequency response for an IDT having fingers, shaped in form of curled brackets, is illustrated in Applicant's Fig. 6a (64).</p>
--	--

In order to help find important key words such "periodicity", "arrangement", "shaped", "configured", etc. in the disclosure description following is included:

(a) Page 8, lines 21-30

In the approach of the variational principle, the SAW velocity is expressed with two terms....The second term is defined by the mechanical load, i.e. by densities and constants both of the piezosubstrate and the electrode finger material, as well as **periodicity** of the fingers and their geometry: thickness and width. Both of the term smoothly with an electrode finger's width. Calculations show that if an electrode finger's thickness is in the range from 25% to 60% of the distance between the adjacent finger's centers, the terms are approximately proportional to the electrode fingers width. So if the electrode fingers change in width along their length, the SAW velocity dispersion is expected to occur in the same direction.

(b) Page 11, lines 23-25

The SAW velocity dispersion depends on both electrical and mechanical load, i.e., it depends on the material both of the piezoelectric substrate and the electrode fingers and depend on the thickness, **configuration**, polarity and **arrangement** of the electrode fingers.

(c) Page 15, lines 24-27

SAW velocity dispersion causes frequency response widening for an inter-digital transducer with electrode fingers which change in width along their length, in contrast to a transducer with conventional electrode fingers, i.e. wherein the fingers are either of uniform width along their length or of width **configured** in alignment with tapering of the transducer.

(d) Page 24 -- Claim 1

A transducer for surface acoustic waves, said transducer comprising a plurality of interdigitized electrode fingers, including at least one interdigitized electrode finger which is provided with a **shape** that changes in width along said finger's length, provided that where a transducer is tapered, said electrode finger width is not uniformly changed to maintain alignment with the tapering of the transducer,...

(e) Page 24 -- Claim 3

A transducer according to claim 1, wherein said electrode fingers are **arranged** without regard to uniformity of **periodicity** along the lengths of electrode fingers.

(f) Page 24 -- Claim 4

A transducer according to claim 1, wherein said electrode fingers are arranged without regard to uniformity of **periodicity** in the direction of the wave propagation through said transducer.

(g) And even General Claim 23:

A SAW transducer having electrode fingers shaped in order to produce a SAW velocity dispersion effect.  
...that assumed any **shaping** to achieve **purposely** the SAW velocity dispersion effect.

**SHIBOLETH, ISRAELI, RUBIN & CO., L.L.C.**  
ADVOCATES, PATENT ATTORNEYS & NOTARY

LIOR AVIRAM  
SAVYON AMIT  
GIL ARIE  
HELENA BEILIN  
RON BEN-MENACHEM  
DAVID BERNHEIM  
RUTH DAGAN  
JONATHAN FEIGIN  
AMIR FISHER  
ALMOG GEVA  
DOV GOVRIN  
MICHAL GOTTESMAN-BARAK  
OREN HEIMAN  
MIRIAM HELLER LIDJI  
ROTEM HARARI  
HILLEL ISH-SHALOM  
DR. YUVAL KARNIEL  
BOAZ LAHOVITSKY

TEL AVIV ADDRESS  
44-46 MONTEFIORE ST., TEL AVIV 65201, ISRAEL TEL: 972-3-7103311, FAX: 972-3-7103322  
e-mail: manager@shiboleth.com WEBSITE: www.shiboleth.com

RAANANA ADDRESS  
312 GIRON CENTER, P.O.B. 410 RAANANA 43103, ISRAEL TEL: 972-9-7713585, FAX: 972-9-7713593

NEW YORK ADDRESS  
EMPIRE STATE BUILDING 350 FIFTH AVENUE, 60th FLOOR  
NEW YORK, N.Y. 10118. TEL: (212) 244-4111, FAX: (212) 563-7108

EDWARD LANGER  
OFER MANOR  
GADI OUZAN  
SHLOMIT OPHIR-HAREL  
LIMOR PELED  
DIKLA PIUDIK  
AVIGDOR RABINOVICH  
DANA RAUCHER  
IDIT REITER  
RICHARD M. ROBERTS  
HAGIT SAMUEL  
OFER SHAPIRA  
AMNON SHIBOLETH  
ORIT STERNHELL-ZALTZMAN  
HAGAI TIOMKIN  
YAACOV YISRAELI  
TALYA YISRAELI  
ITZHAK ZISMAN

**INTELLECTUAL PROPERTY DEPARTMENT**

EDWARD LANGER B.S.E.E., M.B.A., J.D. - ADV. & PAT. ATTY. (Israel Bar), REG. US PAT. ATTY. (Pennsylvania Bar)  
e-mail: e.langer@shiboleth.com

Mr. Peter Medley, Examiner  
US Patent and Trademark Office, Group Art Unit 2834  
Washington, DC 20231

September 23, 2002  
BY FAX (703) 746 4178

Re: US Pat. Appln. S/N 09/685,718

"METHOD UTILIZING THE SAW VELOCITY DISPERSION EFFECT FOR  
WEIGHTING BY SHAPING THE ELECTRODE FINGERS...."

Our file: A-378-0 US

Dear Mr. Medley,

Thank you for the opportunity to discuss the subject matter with you, hopefully we can do this today by telephone at your time 9:00 AM.

I have attached a Power of Attorney form signed by the inventor, adding my name as attorney of record.

I have also attached a proposed new claim (31) and a table of comparison between the prior art and the present invention.

Please review these materials so that we can discuss them today or another convenient time.

A significant point to keep in mind was stated in the earlier response filed by the previous attorney on Jan. 4, 2002. This refers to the fact that the Yatsuda reference does not relate to interdigital transducers nor to the weighting of IDTs. In general, the prior art discloses fingers which are arranged and tapered to compensate for and reduce the effects of velocity dispersion. As he stated in that response, "In stark contrast to the prior art, the finger shaping called for by the present invention is provided for precisely the opposite reason, i.e. in order to induce the velocity dispersion effect, thereby weighting the transducer itself and/or focusing the propagated SAW beam."

It is believed that new claim 31 presents language defining over the prior art with regard to the variable ratio inducing SAW velocity dispersion, to provide a weighting mechanism to control weighting coefficients for achieving desired frequency characteristics of the IDT.

Looking forward to discussing this matter with you.

Sincerely,

  
Edward Langer, Pat. Atty  
Registration No. 30,564